

SEWER SERVICE AREAS

As shown in Figure 3, Service Area Map, the developable portion of the Study Area has been divided into four Service Areas, as follows:

Service Area A is comprised of approximately 1.3 square miles of the Study Area lying to the north of Kimball Avenue. It is bounded to the north by Merrill Avenue, on the east by Carpenter Avenue and County Line, and on the west by the Chino Airport. This Area will be serviced by proposed collector sewers tributary to the Kimball Interceptor Trunk Sewer

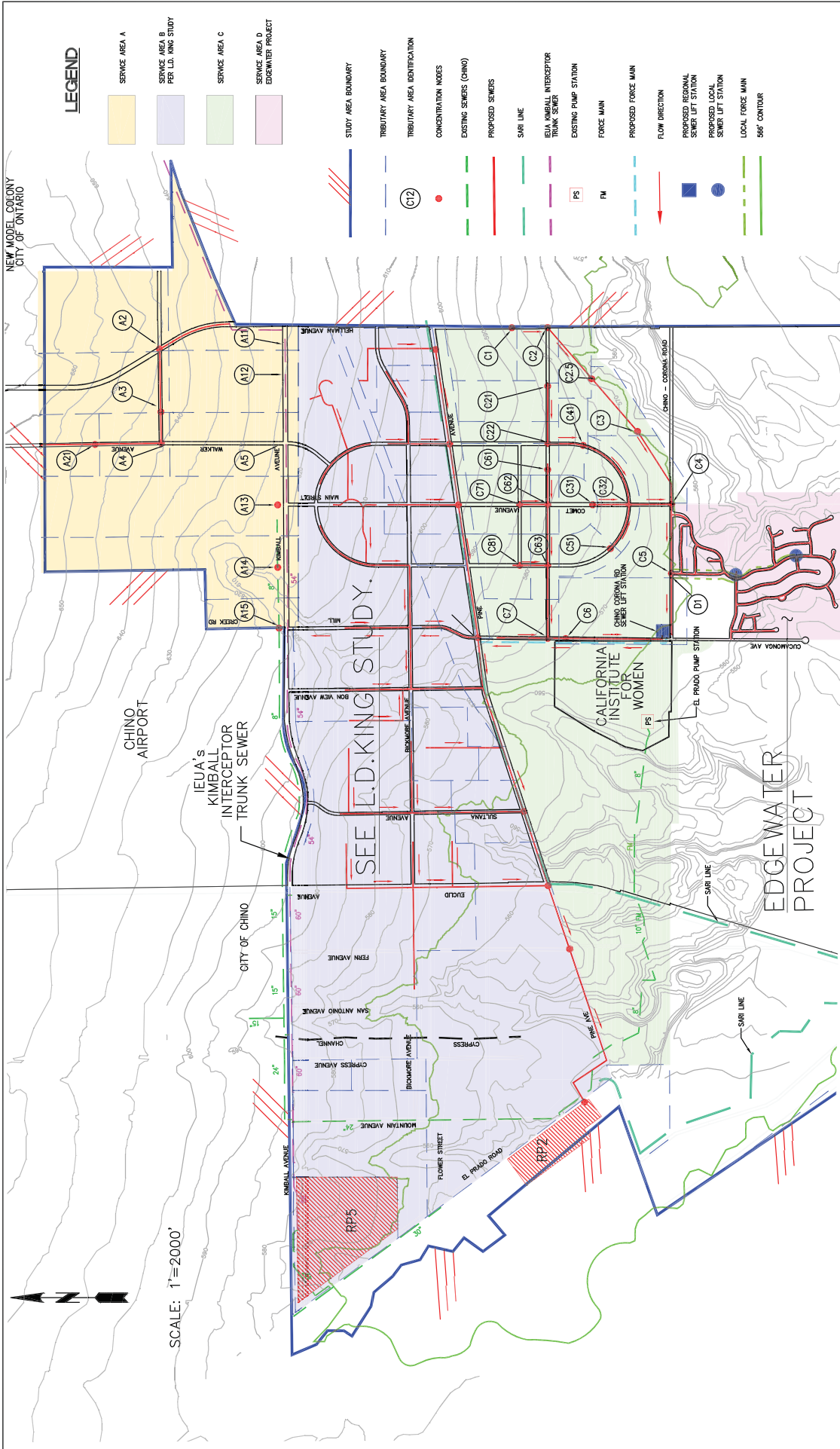
Ground surface in Service Area A is well above the 566-foot elevation and thus outside the limit of the Prado Dam's impoundment area.

The Kimball Interceptor Trunk Sewer is an existing gravity sewer pipeline that extends easterly along Kimball Avenue from RP-5 to Hellman Avenue, then runs northeast along the County Line to Archibald Avenue, thence extends north in Archibald Avenue as the City of Ontario's Eastern Trunk Sewer and IEUA's RP-1/RP-5 By-pass Sewer. It is tabled to convey flows from City of Chino areas lying to the north of Kimball Avenue, City of Ontario's New Model Colony, and to by-pass flows from IEUA's Reclamation Plant No. 1 (RP-1) to RP-5. RP-1 is located in the City of Ontario (at 2662 East Walnut Avenue) and services portion of IEUA's Service Area north of State Route 60.

The Kimball Interceptor Trunk Sewer has the capacity to convey flows generated from its tributary watershed and RP-1/RP-5 By-pass flows, for the built-out condition. In the interim this sewer has excess capacity and can be utilized to convey flows from areas south of Kimball Avenue, if needed to accommodate sequencing of piece-meal development verses scheduling of implementation of downstream master planned facilities.

Service Area B is the portion of the Study Area between Kimball Avenue and Pine Avenue, bounded by Hellman Avenue in the east and El Prado Road in the west. This Service Area is comprised of an approximately 3.4 square mile area that will be tributary to IEUA's RP-2 Regional Pumping Facility via a gravity trunk sewer along Pine Avenue (proposed Pine Avenue Trunk Sewer), as recommended in the LD King Study.

Except for the sewer sizes in Pine Avenue west of Cucamonga Avenue/Mill Creek Road (see Service Area C), sizes, alignments and flow rates for the master planned backbone facilities for Service Area B are based on the LD King Study.



LEGEND

- SERVICE AREA A
- SERVICE AREA B PER L.D. KING STUDY
- SERVICE AREA C
- SERVICE AREA D EDGEWATER PROJECT

- STUDY AREA BOUNDARY
- TRIBUTARY AREA BOUNDARY
- TRIBUTARY AREA IDENTIFICATION
- CONCENTRATION NODES
- EXISTING SEWERS (CHNO)
- PROPOSED SEWERS
- SARI LINE
- EIUA KIMBALL INTERCEPTOR TRUNK SEWER
- EXISTING PUMP STATION
- FORCE MAIN
- PROPOSED FORCE MAIN
- FLOW DIRECTION
- PROPOSED REGIONAL SEWER LIFT STATION
- PROPOSED LOCAL SEWER LIFT STATION
- LOCAL FORCE MAIN
- 566' CONTOUR

SERVICE AREA MAP

**CITY OF CHINO
SUBAREAS 1 AND 2**

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SEWER MASTER PLAN UPDATE REPORT

FIGURE NO. 3

Service Area C is comprised of an area of approximately 1.2 square miles lying to the south of Pine Avenue, and bounded by Chino Corona Road to the south, Cucamonga Avenue/Mill Creek Road to the west, and by the Riverside County Line to the east. As recommended in the LD King Study, this area will be serviced by the proposed gravity sewer lines which will convey flows to the proposed Chino Corona Road Sewer Lift Station to be located at the northeast corner of Chino Corona Road and Cucamonga Avenue/Mill Creek Road.

There are two alternatives for the conveyance of flows from Corona Chino Road Lift Station to RP-5, as follows:

- **Alternative 1:** As recommended in the LD King Study, flows from Chino Corona Road Sewer Lift Station are to be pumped to the existing Kimball Interceptor Trunk Sewer, in a 12-inch force-main along Cucamonga Avenue/Mill Creek Road.

This is a viable solution if development in Service Area C is to occur prior to the construction of the proposed trunk sewer in Pine Avenue which is needed for the development in Service Area B.

- **Alternative 2:** Alternatively, flows from Chino Corona Road Sewer Lift Station can be pumped to the future Pine Avenue Trunk Sewer, which would convey the flows to RP-2 along with flows generated in Service Area B.

This Alternative would increase the sizes for a portion of the proposed Pine Avenue Trunk Sewer, but would eliminate the need to construct the force-main between Pine Avenue and Kimball Avenue.

Comparison of preliminary construction cost estimates for the impacted portion of the proposed Pine Avenue Trunk Sewer and the proposed force-main under the two alternatives has been summarized in Table 7, included in the Cost Estimates Section of this report. Based on this evaluation, Alternative 2 is the most cost effective option.

Service Area D is comprised of approximately 0.3 square miles of the Study Area lying to the south of Chino Corona Road and east of Cucamonga Road, proposed for residential and open space development as the Edgewater Development. A significant portion of Service Area D is below the 566-foot "High Water Elevation" of the Prado Flood Control Basin.

The Edgewater Development will be serviced by local collection systems accompanying two lift stations as described per Huitt-Zollars' updated report for Edgewater Development, dated March 2007. The local Lift Stations will convey flows to the Chino Corona Road Sewer Lift Station.

At build-out condition of the Land Use Plan, approximately twenty percent (20%) of the projected average daily flows tributary to Chino Corona Road Sewer Lift Station will be generated by the Edgewater Development and eighty percent (80%) by Service Area C.

FLOW PROJECTIONS

Based on a review of unit wastewater flow generation factors used in the City of Chino's Sewer Master Plan, and those used by neighboring cities and by the Inland Empire Utilities Agency, the following factors were used for the development of average sewer flows generated within the Study Area.

Flow projections for the Residential Land Uses are based on an average daily flow generation of 80 gallons per day per person. The average estimated density in the study area is approximately 3.4 persons per dwelling unit (DU), based on The Preserve Specific Plan dated March 2003.

Projected average daily flows in gallons per day per gross acre (gpd/acre) for each Land Use type are as follows:

<u>Residential Land Use Type</u>	<u>Average DUs/acre</u>	<u>Average Daily Flows Rate</u>
Estate	2	536 gpd/acre
Low Density	5.25	1,412 gpd/acre
Medium Density:	9	2,395 gpd/acre
High Density:	13.5	3,642 gpd/acre
Commercial:		2,500 gpd/acre
Offices:		2,000 gpd/acre.
Industrial (Light):		1,000 gpd/acre
Public Facilities:	Institutional: 2500 gpd/acre Airport: 1000 gpd/acre	
Open Space:	Recreational: 100 gpd/acre Natural: 0	
Agricultural:		1,000 gpd/acre (to account for some future change in land use)

A breakdown of acreage for each Land Use type, and flow projections at build-out conditions have been summarized in Table 1 for Service Area A; and in Table 2 for Service Areas B, C, and D. Flow rates and facility sizes for Service Area B are based on the L.D. King Study report.

TABLE 1

LAND USE DISTRIBUTION - SERVICE AREA A

Land Use Classification	Residential				Commercial					Industrial		Public Facilities		Open Space		Agricultural	TOTAL ACRES	Average Flows (gpd)	
	ER	LDR	MDR	HDR	RC	CC	AR	NC	LI	INS	AP	OS - R	AG						
Flow Factors	536	1412	2395	3642	2500	3050	2500	2500	1000	2500	1000	100	1000						
Trib Areas																			
A15			2.9				1.3				11.0						15.1	21,036	
A14			6.2				28.0				82.3						116.5	187,221	
A13			5.9				27.9				126.3						160.0	209,886	
A21									18.1		18.8						36.9	36,890	
A2									3.4						23.2		3.4	26,520	
A4									21.0		32.5						53.6	53,610	
A3									76.6								76.6	76,620	
A5			6.6				22.4		25.0		20.8						74.8	117,500	
A12			6.4				18.7		53.9								79.0	116,029	
A11			1.0				7.2	1.8	17.0							51.6	26.9	93,271	
Total	0.0	0.0	28.9	0.0	0.0	0.0	105.5	1.8	214.9	0.0	291.8	0.0	74.7	0.0	0.0	717.5	918,583		

ER = ESTATE RESIDENTIAL

LDR = LOW DENSITY RESIDENTIAL

MDR = MEDIUM DENSITY RESIDENTIAL

HDR = HIGH DENSITY RESIDENTIAL

RC = REGIONAL COMMERCIAL

CC = COMMUNITY CORE

AR = AIRPORT RELATED COMMERCIAL

NC = NEIGHBORHOOD COMMERCIAL

LI = LIGHT INDUSTRIAL

INS = INSTITUTIONAL

AP = AIRPORT

OS-R = OPEN SPACE - RECREATIONAL

AG = AGRICULTURAL

TABLE 2

LAND USE DISTRIBUTION - SERVICE AREAS C AND D

Land Use Classifications	Residential						Commercial						Office		IND		Public Facilities		Open Space		Agricultural		Total ACRES	Average Flows (gpd)
	ER	LDR	MDR	HDR	RC	CC	AR	NC	BP/O	LI	INS	AP	OS - R	AG	AG	INS	AP	OS - R	AG	AG				
	536	1412	2395	3642	2500	3050	2500	2500	2000	1000	2500	1000	100	1000	1000	2500	1000	100	1000	1000	1000			
Trib Areas																								
C7		3.68	21.82				1.62									0.16		2.93					30.21	62,198
C81			16.25	15.77																			32.02	96,353
C71						32.93																	32.93	100,437
C81				27.39																			27.39	99,754
C21	1.48	2.31	39																				42.79	97,460
C22		2.02	18.52																				20.54	47,208
C1		37.04																					37.04	52,300
C2	5.38	15.79																					21.17	25,179
C2.5	20.76																	3.53					24.29	11,480
C83		3.17	5.24	7.67																			16.08	44,960
C62						14.2																	14.2	43,310
C6	25.51	50.68																					83.5	96,045
C5	25.23	12.93																	4.2				46.33	32,597
C51		6.45		14.4																			20.85	61,552
C32		12.71	18.2	7.18																			38.09	87,685
C31						18.29																	18.29	55,785
C41		13.73		8.2																			21.93	49,251
C3	18.58	4.93																					37.76	18,345
C4	10.69	6.86																					29.39	16,600
D1		63.82	28.7	15.63																			150.07	219,967
D2		33.94																					63.41	50,870
TOTALS	107.63	270.06	147.73	96.24	0	65.42	0	1.62	0	0	0	0	0	0	4.36	0	0	115.22	0	0	0	808.28	1,369,337	

ER = ESTATE RESIDENTIAL
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 MDR = MEDIUM DENSITY RESIDENTIAL
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DESIGN CRITERIA

Average flows were routed in the proposed sewer facilities. The proposed backbone facilities' sizes are based on tributary peak dry weather flows using the peaking factor formula developed in the City of Chino's Sewer Master Plan:

$$\text{Dry Weather Peaking Factor (DWPF)} = 1.95 \times (\text{Average Flow [in cfs]})^{-0.038}$$

$$\text{Peak Dry Weather Flow} = (\text{DWPF}) \times (\text{Average Flow})$$

Hydraulic criteria for sizing of pipes is based on Manning's Equation with a Manning's Coefficient $n = 0.013$.

Pipe material for gravity sewer: Extra Strength Vitrified Clay Pipe with rubber gaskets.

Minimum velocity in gravity sewer: 2 feet per second

Minimum slopes: (gravity sewers)	For 6-inch diameter pipe	0.0100
	For 8-inch diameter pipe	0.0040
	For 10-inch diameter pipe	0.0030
	For 12-inch diameter pipe	0.0024
	For 15-inch diameter pipe	0.0017
	For 18-inch diameter pipe	0.0014
	For 21-inch diameter pipe	0.0011
	For 24-inch diameter pipe	0.0010
	For 27-inch diameter pipe	0.0010

Maximum ratio of flow depth to pipe diameter (d/D ratio) for peak flows in gravity sewer is as follows:

- 0.50 for pipe diameter less than 12 inches.
- 0.67 for pipe diameter equal to 12 inches.
- 0.75 for pipe diameter greater than 12 inches.

Sewer systems in the impoundment areas should be designed as sealed systems to mitigate the potential of high inflow and infiltration into the sewer system. All manhole covers and clean-out covers with elevations lower than 566 feet should have bolted covers with pressure plated assemblies. All sewer structures including wet wells, junction structures, flow splitters and manholes that extend below the 566-foot elevation shall be plastic lined, and include water-stops at all construction and expansion joints.

Summary of hydraulic parameters for the recommended sewer reaches within Service Area A is included in Table 3, and for Service Areas C and D in Table 4. Table 5 summarizes the hydraulic parameters for the Pine Avenue Trunk Sewer, from Cucamonga Avenue/Mill Creek Road to IEUA's Pumping Facility at RP-2.

BACKBONE FACILITIES

Proposed backbone facilities for the built-out condition of the Study Area are shown in Figure 4, Facilities Map. Sizes and alignments for the recommended facilities are for master planning purposes, based on preliminary evaluation of the Study Area. Final design of the proposed facilities should incorporate design details and phasing of the future developments and other infrastructure.

Proposed 8-inch sewers shown on the map are for planning purposes. Sewers with less than 10-inch diameter are not considered to be master planned backbone facilities.

TABLE 3

HYDRAULIC CALCULATION - SERVICE AREA A

REACH NO.	AREA	AVERAGE Q (GPD)	AVERAGE Q (CFS)	PEAK FACTOR	PEAK FLOW (CFS)	PEAK FLOW (MGPD)	SLOPE (%)	D/d	V (FPS)	SIZE (IN)
152	A21	36,890	0.0571	2.17	0.1241	0.0802	1	0.22	2.23	8
153	A21,A4	90,500	0.1400	2.10	0.2942	0.1902	0.7	0.37	2.51	8
154	A21,A4,A3	167,120	0.2586	2.05	0.5308	0.3431	0.4	0.43	2.37	10
155	A21,A4,A3,A2	193,640	0.2996	2.04	0.6116	0.3953	0.3	0.39	2.20	12

TABLE 4

HYDRAULICS CALCULATIONS - SERVICE AREAS C AND D

REACH NO.	AREA	AVERAGE Q (GPD)	AVERAGE Q (CFS)	PEAK FACTOR	PEAK FLOW (CFS)	PEAK FLOW (MGPD)	SLOPE (%)	D/d	V (FPS)	SIZE (IN)
108	C7	62,198	0.0962	2.13	0.2051	0.1326	0.6	0.32	2.14	8
128	C81	96,353	0.1491	2.10	0.3125	0.2020	0.47	0.42	2.20	8
127	C71	100,437	0.1554	2.09	0.3252	0.2102	0.78	0.38	2.68	8
124	C61,C62,C71, C81,C63	384,814	0.5954	1.99	1.1841	0.7653	0.25	0.60	2.43	12
125	C61,C62,C71	243,501	0.3767	2.02	0.7624	0.4928	0.35	0.42	2.47	12
126	C61, C61,C62,C71,C81,C6 3,C7	99,754	0.1543	2.09	0.3231	0.2088	0.7	0.39	2.28	8
140	C61,C62,C71,C81,C6 3,C7	447,012	0.6916	1.98	1.3677	0.8840	0.4	0.56	3.00	12
129	C61,C62,C71,C81,C6 3,C7,C6	543,057	0.8402	1.96	1.6493	1.0660	0.2	0.54	2.43	15
130	C21,C22,C41,C31,C5 1,C32,C1,C2,C2.5,C5 ,C3,C4	555,443	0.8594	1.96	2.5459	1.6455	0.14	0.59	2.36	16
	D1	219,987	0.3403	2.03						
	D2	50,870	0.0787	2.15						
131	C21,C22,C41,C31,C5 1,C32,C1,C2,C2.5,C5 ,C3,C4	555,443	0.8594	1.96	1.6855	1.0894	0.17	0.58	2.29	15
132	C21,C22,C41,C31 ,C51,C32	398,941	0.6172	1.99	1.2259	0.7923	0.25	0.61	2.44	12
133	C21,C22,C41	193,919	0.3000	2.04	0.6125	0.3958	0.4	0.47	2.46	10
137	C21,C22, C21	144,668	0.2238	2.06	0.4620	0.2986	0.5	0.38	2.48	10
110	C21, C1,C2,C2.5	97,460	0.1508	2.10	0.3160	0.2042	0.65	0.49	2.49	8
112	C1,C2,C2.5 C1,C2	88,960	0.1376	2.10	0.2894	0.1870	0.7	0.37	2.50	8
139	C1,C2 C1	77,480	0.1199	2.11	0.2534	0.1638	0.7	0.34	2.41	8
138	C1 C31	52,300	0.0809	2.15	0.1736	0.1122	1.25	0.24	2.66	8
134	C31	55,785	0.0863	2.14	0.1847	0.1194	1.67	0.23	2.95	8
135	C51	61,552	0.0952	2.13	0.2031	0.1312	0.76	0.27	2.23	8
136	C1,C2,C2.5,C3	107,305	0.1660	2.09	0.3466	0.2240	0.6	0.31	2.44	10
TOTAL:		1,098,500	1.6996	1.91	3.2481	2.0993				

TABLE 5

HYDRAULICS CALCULATIONS - PINE AVE TRUNK SEWER FROM MILL CREEK ROAD TO RP2

REACH NO.	AVERAGE Q FROM LDK STUDY (GPD)	AVERAGE Q FROM LDK STUDY (CFS)	PEAK FACTOR	PEAK FLOW (CFS)	ADDITIONAL FLOW FROM AREAS C & D (CFS)	TOTAL PEAK FLOW (CFS)	PEAK FLOW (MGPD)	SLOPE (%)	D/d (%)	V (FPS)	SIZE (IN)
37	525,628	0.81	1.97	1.60	4.1952	5.79	1.0331	0.2917	0.61	3.81	21
39	1,396,597	2.16	1.89	4.09	4.1952	8.29	2.6448	0.2917	0.61	4.17	24
41	1,549,063	2.40	1.89	4.52	4.1952	8.72	2.9220	0.2917	0.62	4.22	24
50	1,788,084	2.77	1.88	5.19	4.1952	9.39	3.3545	0.2917	0.66	4.27	24
51	1,862,077	2.88	1.87	5.40	4.1952	9.59	3.4879	0.2917	0.67	4.30	24
58	2,565,559	3.97	1.85	7.35	4.1952	11.54	4.7475	0.2	0.70	3.90	27
61	2,713,699	4.20	1.85	7.75	4.1952	11.95	5.0109	0.2	0.72	3.92	27

SCALE: 1" = 2000'

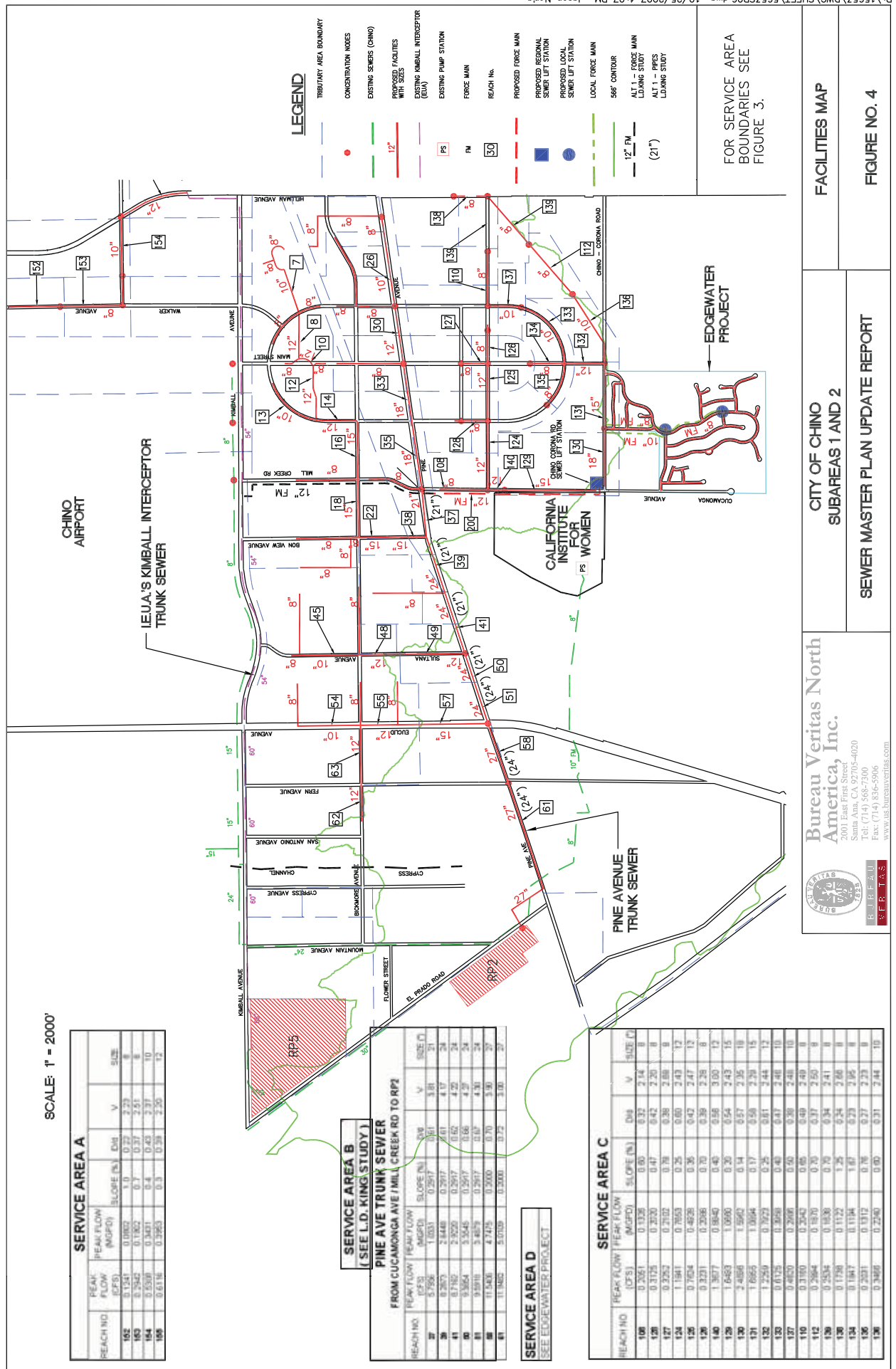
SERVICE AREA A					
REACH NO.	PEAK FLOW (MGPD)	PEAK FLOW (MGPD)	SLOPE (%)	DIA	SIZE (V)
162	0.1341	0.0862	1.0	0.25	2.25
163	0.2342	0.1562	0.7	0.37	2.51
164	0.5308	0.3401	0.4	0.43	2.37
165	0.6116	0.3963	0.3	0.58	2.20

SERVICE AREA B
(SEE L.D. KING STUDY)

PINE AVE TRUNK SEWER FROM CUCAMONGA AVE / MILL CREEK RD TO RP2					
REACH NO.	PEAK FLOW (MGPD)	PEAK FLOW (MGPD)	SLOPE (%)	DIA	SIZE (V)
37	0.7556	1.0231	0.2517	0.51	3.81
38	0.2670	2.8448	0.2917	0.61	4.17
41	0.7182	2.9209	0.2917	0.62	4.20
42	0.9364	3.3445	0.2917	0.66	4.30
43	0.9391	3.4879	0.2917	0.67	4.30
44	11.8403	4.7415	0.2000	0.70	3.90
45	11.8403	5.0749	0.2000	0.72	3.90

SERVICE AREA D
SEE EDGEWATER PROJECT

SERVICE AREA C					
REACH NO.	PEAK FLOW (MGPD)	PEAK FLOW (MGPD)	SLOPE (%)	DIA	SIZE (V)
108	0.2361	0.1326	0.80	0.32	2.14
109	0.1125	0.2320	0.47	0.42	2.20
107	0.2257	0.2102	0.78	0.38	2.08
104	1.1841	0.7653	0.25	0.60	2.43
105	0.7924	0.4928	0.35	0.42	2.47
106	0.3231	0.2088	0.70	0.39	2.28
140	1.3677	0.8840	0.45	0.56	3.00
126	1.6483	1.0690	0.26	0.54	2.43
130	2.4856	1.5940	0.14	0.57	2.35
131	1.8653	1.0684	0.17	0.58	2.39
132	1.2256	0.7923	0.24	0.61	2.44
133	0.1125	0.2090	0.45	0.43	2.48
137	0.4620	0.2907	0.60	0.38	2.48
110	0.1180	0.2540	0.65	0.40	2.40
112	0.2864	0.1630	0.70	0.37	2.50
108	0.2534	0.1636	0.70	0.34	2.41
106	0.1758	0.1122	1.25	0.24	2.66
134	0.1947	0.1134	1.67	0.23	2.95
136	0.2031	0.1312	0.76	0.27	2.73
136	0.3460	0.2240	0.60	0.31	2.44



FOR SERVICE AREA BOUNDARIES SEE FIGURE 3.

FACILITIES MAP

FIGURE NO. 4

CITY OF CHINO
SUBAREAS 1 AND 2

SEWER MASTER PLAN UPDATE REPORT

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COST ESTIMATES

Estimates for construction and project costs have been developed for each reach of sewer shown on the Facilities Map, as summarized in Table 6.

Proposed 8-inch diameter sewers shown on the Facilities Map are for planning purposes only. The costs associated with 8-inch diameter sewers has not been included in the cost estimates summarized in Table 6, since construction of 8-inch diameter sewers will be the responsibility of the developers.

The construction cost estimates are based on an ENR Construction Cost Index of 7,865, and incorporate a contingency of 20%. The capital costs include 10% of construction costs for engineering and administration.

TABLE 7

COST COMPARISON OF ALTERNATIVES

		ALTERNATIVE 1					ALTERNATIVE 2						
		Pumping flows from Chino Corona Road Sewer Lift Station to existing Kimball Interceptor Trunk Sewer					Pumping flows from Chino Corona Road Sewer Lift Station to proposed Pine Avenue Trunk Sewer						
REACH	No.	SIZE	LENGTH	UNIT	CONSTRUCTION	SIZE	LENGTH	UNIT	CONSTRUCTION	SIZE	LENGTH	UNIT	CONSTRUCTION
		(in)	(feet)	COST	COST	(in)	(feet)	COST	COST	(in)	(feet)	COST	COST
Pine Avenue Trunk Sewer Segment, downstream of Cucamonga Avenue.	37*	21	1090	\$311	\$338,990	21	1090	\$311	\$338,990	21	1090	\$311	\$338,990
	39*	21	1360	\$311	\$422,960	24	1360	\$345	\$469,200	24	1360	\$345	\$469,200
	41*	21	1450	\$311	\$450,950	24	1450	\$345	\$500,250	24	1450	\$345	\$500,250
	50*	21	700	\$311	\$217,700	24	700	\$345	\$241,500	24	700	\$345	\$241,500
	51*	24	990	\$345	\$341,550	24	990	\$345	\$341,550	24	990	\$345	\$341,550
	58*	24	1430	\$345	\$493,350	27	1430	\$379	\$541,970	27	1430	\$379	\$541,970
61*	24	3860	\$345	\$1,331,700	27	3860	\$379	\$1,462,940	27	3860	\$379	\$1,462,940	
FM	200	12	8350	\$175	\$1,461,250	12	4000	\$180	\$720,000	12	4000	\$180	\$720,000
		Alternative 1 Cost: \$ 5,058,450					Alternative 2 Cost: \$ 4,616,400						

* - pipes below 566' contour

TABLE 6**COST ESTIMATES**

REACH NO.	SIZE (in)	LENGTH (feet)	UNIT COSTS	CONSTRUCTION COSTS	ENGR/ ADMIN	TOTAL CAPITAL COSTS
7	10	1100	\$179	\$196,900	\$19,690	\$216,590
8	12	1070	\$198	\$211,860	\$21,186	\$233,046
10	12	450	\$198	\$89,100	\$8,910	\$98,010
12	12	1230	\$198	\$243,540	\$24,354	\$267,894
13	10	1350	\$179	\$241,650	\$24,165	\$265,815
14	12	960	\$198	\$190,080	\$19,008	\$209,088
16	15	1320	\$225	\$297,000	\$29,700	\$326,700
18	15	1340	\$225	\$301,500	\$30,150	\$331,650
22	15	800	\$225	\$180,000	\$18,000	\$198,000
38*	15	800	\$250	\$200,000	\$20,000	\$220,000
26	10	1410	\$179	\$252,390	\$25,239	\$277,629
30	12	1330	\$198	\$263,340	\$26,334	\$289,674
33	18	1330	\$254	\$337,820	\$33,782	\$371,602
35	18	1570	\$254	\$398,780	\$39,878	\$438,658
37*	21	1090	\$311	\$338,990	\$33,899	\$372,889
39*	24	1360	\$345	\$469,200	\$46,920	\$516,120
41*	24	1450	\$345	\$500,250	\$50,025	\$550,275
45	10	1360	\$179	\$243,440	\$24,344	\$267,784
48*	12	845	\$223	\$188,435	\$18,844	\$207,279
49*	12	1555	\$223	\$346,765	\$34,677	\$381,442
50*	24	700	\$345	\$241,500	\$24,150	\$265,650
51*	24	990	\$345	\$341,550	\$34,155	\$375,705
54	10	1430	\$179	\$255,970	\$25,597	\$281,567
55*	12	848	\$223	\$189,104	\$18,910	\$208,014
57*	15	2060	\$250	\$515,000	\$51,500	\$566,500
62*	12	847	\$223	\$188,881	\$18,888	\$207,769
63*	12	1357	\$223	\$302,611	\$30,261	\$332,872
58*	27	1430	\$379	\$541,970	\$54,197	\$596,167
61*	27	3860	\$379	\$1,462,940	\$146,294	\$1,609,234
137	10	770	\$179	\$137,830	\$13,783	\$151,613
133*	10	1730	\$204	\$352,920	\$35,292	\$388,212
132*	12	920	\$223	\$205,160	\$20,516	\$225,676
136*	10	1780	\$204	\$363,120	\$36,312	\$399,432
131*	15	1500	\$250	\$375,000	\$37,500	\$412,500
130*	18	1400	\$279	\$390,600	\$39,060	\$429,660
129*	15	2230	\$250	\$557,500	\$55,750	\$613,250
140*	12	390	\$223	\$86,970	\$8,697	\$95,667
124	12	1580	\$198	\$312,840	\$31,284	\$344,124
125	12	1310	\$198	\$259,380	\$25,938	\$285,318
154	10	1380	\$179	\$247,020	\$24,702	\$271,722
155	12	1620	\$198	\$320,760	\$32,076	\$352,836
200	12	4000	\$180	\$720,000	\$72,000	\$792,000
PS		LS		\$3,000,000	\$500,000	\$3,500,000
TOTALS		57852		\$ 16,859,666	\$ 1,885,967	\$ 18,745,633

* - pipes below 566' contour

K.5 - Storm Drain Master Plan Update Report
Prepared by Bureau Veritas - Draft Final Report November 2007



**BUREAU
VERITAS**

Bureau Veritas North America, Inc.

Storm Drain

Master Plan Update Report

Subarea 2

Chino Agricultural Preserve Area



**City of
Chino**

**Final Report
December 2007**

STORM DRAIN MASTER PLAN UPDATE REPORT

CITY OF CHINO - SUBAREA 2

CHINO AGRICULTURAL PRESERVE AREA

Prepared for:

City of Chino
13220 Central Avenue
Chino, CA 91710

Prepared by:

Bureau Veritas, North America, Inc.
2001 East First Street
Santa Ana, CA 92705

Prepared Under the Supervision of:



Mohammed Rowther, P.E.

12/17/07

Date



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STORM DRAIN MASTER PLAN UPDATE REPORT

*CITY OF CHINO – SUBAREA 2
CHINO AGRICULTURAL PRESERVE*

INTRODUCTION

This report is an update of the City of Chino's Master Plan of Drainage for Subarea 2 - Chino Agricultural Preserve Area, prepared by Berryman and Henigar dated October 2003. This Update Report incorporates the following:

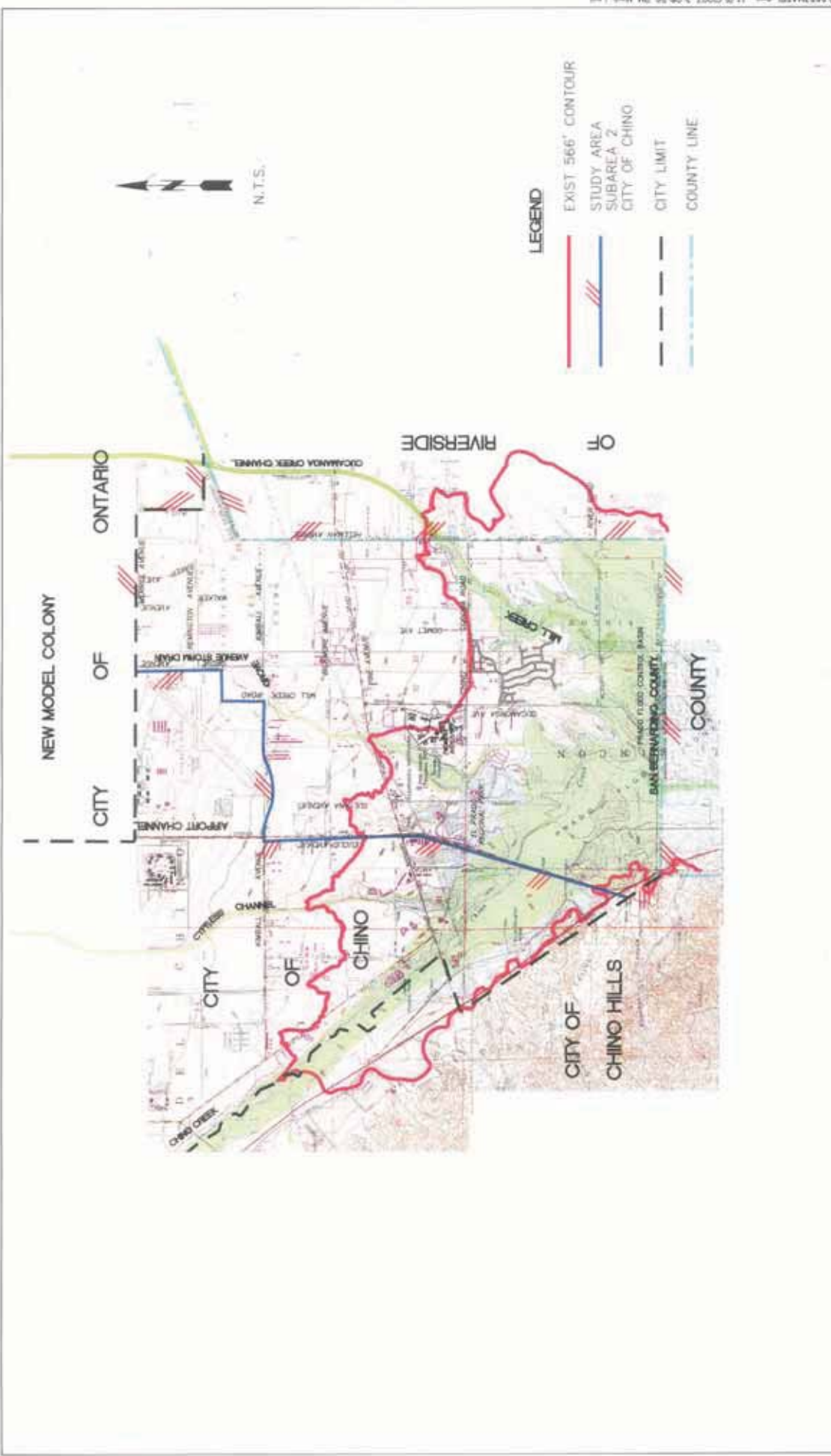
- The proposed Edgewater Development, an approximately 272 acres residential and open space development proposed in Subarea 2 at the south east corner of Chino Corona Road and Cucamonga Avenue.
- Revisions to Master Plan Drainage Basins "B", "D" and "J", as included in the Amendment to Master Plan of Drainage for Subarea 2, prepared by L.D. King, dated July 8, 2004. The Amendment was approved by the City on September 04, 2004.

This Update Report presents preliminary sizes, alignments and cost estimates for recommended backbone drainage facilities required to support full built-out condition of the Study Area. Recommendations included herein are for master planning purposes only. Specific Plans, detailed drainage studies and final design of specific development projects could modify the recommendations of this study.

STUDY AREA

As shown in Figure 1, the Study Area is located in the southwest corner of the County of San Bernardino, and is bounded by Euclid Avenue in the City of Chino to the west, Kimball Avenue and Merrill Avenue to the north, Hellman Avenue to the east, and Riverside County Line through Prado Regional Park to the south.

The Study Area encompasses approximately 8.8 square miles of agricultural and open space property adjacent to Cucamonga Creek Channel, and upstream of the U.S. Army Corp of Engineers' Prado Flood Control Basin. The ground surface in this area generally slopes from north to south, with over half (approximately 4.5 square miles) the Study Area lying below the existing 566' High Water Elevation of the Prado Basin.



 <p>Bureau Veritas North America, Inc. <small>10000 North Central Expressway Suite 1000, Dallas, TX 75243-2098 Tel: (972) 966-7000 Fax: (972) 966-7001 www.bureauveritas.com</small></p>	<p>CITY OF CHINO SUBAREA 2</p>	<p>STUDY AREA MAP</p>
<p>STORM DRAINAGE MASTER PLAN UPDATE REPORT</p>		<p>FIGURE NO. 1</p>

Portion of the Study Area that is below the 566-foot elevation is presently within the impoundment area of the Prado Dam, and therefore can potential be flooded with ponding stormwater during major storm events. However, on-site re-grading of future projects, such as the Edgewater Development, can modify the impoundment area as long as any impacts to the downstream areas or to the Prado Basin, resulting from the re-grading, are mitigated as a part of the project.

LAND USE

The study is based on ultimate built-out condition of the approved land use plan shown in Figure 2, Land Use Map.

HYDROLOGIC CRITERIA

This master plan study has been prepared in conformance with the hydrological procedures and standards set forth in the San Bernardino County Hydrology Manual, 1986 Revision.

Based on the size of each tributary drainage area, the Rational Method or the Unit Hydrograph method was used to calculate the peak runoff at each concentration node. The 100 year frequency storm events were used to determine design peak flows for sizing drainage facilities.

Surface characteristics of pervious areas were based on ultimate development (built-out according to land use maps), having good urban covers (well landscaped), and an average antecedent moisture condition (AMC) II.

Point rainfall data was based on the Isohyetal Maps for Valley Areas, as provided in San Bernardino County Hydrology Manual.

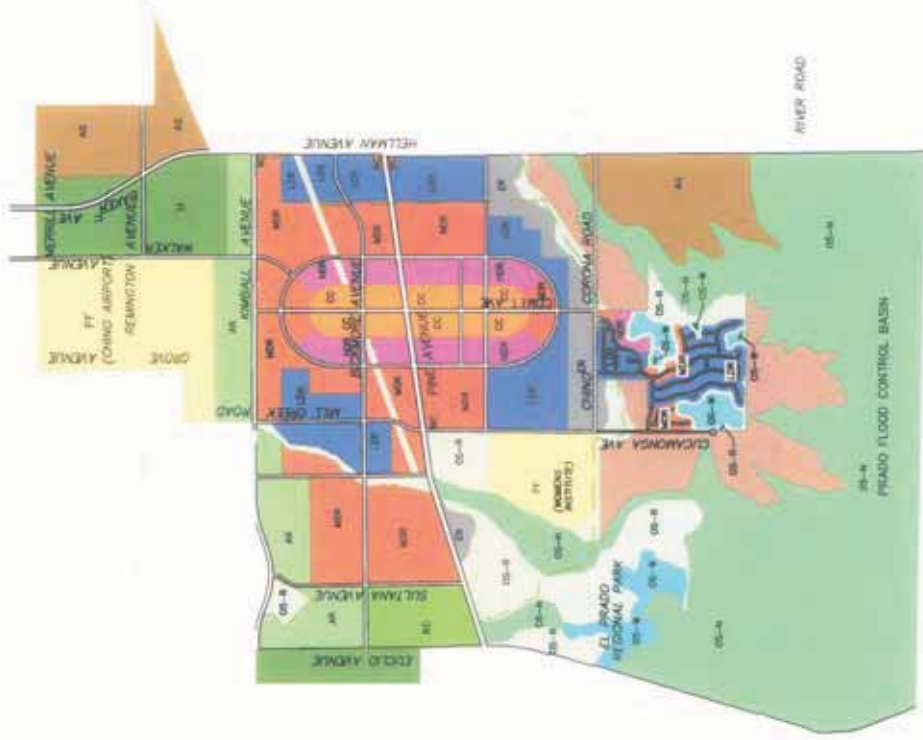
HYDRAULIC CRITERIA

The hydraulic criteria outlined in this section are to be used as a guide to be followed for the final design of storm drain facilities in the Study Area. This criteria has been used to the extent applicable in this master plan study.

1. Hydraulic calculations shall be in accordance with "Los Angeles County Flood Control District Design Manual, Hydraulic", dated March 1982.
2. Closed conduits may be designed as flowing full and may be allowed to flow under pressure if the hydraulic grade line is sufficiently below the ground surface to intercept flows with a minimum freeboard at the catch basin of six (6) inches below the gutter flow lines.

LEGEND

- ER - ESTATE RESIDENTIAL
- LDR - LOW DENSITY RESIDENTIAL
- MDR - MEDIUM DENSITY RESIDENTIAL
- HDR - HIGH DENSITY RESIDENTIAL
- NC - NEIGHBORHOOD COMMERCIAL
- RC - REGIONAL COMMERCIAL
- CC - COMMUNITY CORE
- LI - LIGHT INDUSTRIAL
- AR - AIRPORT RELATED
- PF - PUBLIC FACILITY
- OS-R - OPEN SPACE-RECREATION
- OS-N - OPEN SPACE-NATURAL
- OS-W - OPEN SPACE-WATER
- AG - AGRICULTURE
- AG/OS-N - AGRICULTURE AND OPEN SPACE-NATURAL
- PROPOSED STREETS
- CHURCH - SCHOOL - AREA 8
- PRIVATE RECREATIONAL FACILITY - AREA 7



SCALE: 1" = 3000'

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 Fax: 303.440.2001
 www.bureauveritas.com



CITY OF CHINO
 SUBAREA 2

STORM DRAINAGE MASTER PLAN UPDATE REPORT

LAND USE MAP

FIGURE NO. 2

3. Design velocities in the mainline storm drain conduits shall not exceed forty (40) feet per second (fps). For velocities from twenty (20) to thirty (30) fps, the minimum concrete cover over the reinforcing steel in the pipe shall be one-half (1/2) inch greater than the normal cover (1 1/2 inches minimum). For velocities from thirty (30) to forty (40) fps, the minimum concrete cover over the reinforcing steel in the pipe shall be one (1) inch greater than the normal cover (2 inches minimum).
4. Minimum spacing between manholes shall be follows:
 - a. For conduit thirty (30) inches or smaller, manholes shall be spaced at intervals of approximately three hundred (300) feet. Where the proposed pipe is less than thirty (30) inches in diameter and the horizontal alignment has numerous bends or angle points, the manhole spacing shall be reduced to approximately two hundred (200) feet.
 - b. For conduit diameter greater than thirty (30) inches but smaller than forty five (45) inches, manholes shall be spaced at intervals of approximately four hundred (400) feet.
 - c. For conduit diameter forty-five (45) inches or larger, manholes shall be spaced at maximum intervals of five hundred (500) feet.
5. Pressure manhole shaft and pressure frame and cover shall be used whenever the design water surface (Hydraulic Grade Line) in the storm drain is at or above the finish ground elevation.
6. Covers, lids, and grates for all drainage structures including manholes, junction structures, transitions structures and catch basins, at elevations below 566 feet shall be securely bolted to their frames.
7. The minimum diameter of mainlines and lateral drains shall be 24 inches, and catch basin connector pipe shall be eighteen (18) inches. In cases where the pipe may carry significant amounts of debris, the minimum diameter of mainline pipes shall be thirty-six (36) inches.
8. Minimum slope for mainline storm drains shall be 0.1%, and 0.3% for connector pipes. In cases where the pipe may carry significant amounts of debris, the minimum slope shall be 0.3%.
9. For storm drains that outlet into earthen channels, outlet structures shall be provided to prevent erosion and property damage. Velocity of flow at

the outlet should equal as closely as possible with the existing channel velocity. When the discharge velocity is low or sub-critical, the outlet structures shall consist of a headwall, wing-walls, and apron. When the discharge velocity is high or supercritical, an appropriate energy dissipater and bank protection structure shall be designed in the vicinity of the outlet.

10. If development occurs in the upstream areas prior to construction of the downstream storm drain facilities, local detention basin(s) should be implemented to handle the additional flows generated from such development. The detention basins shall be designed to retard the discharge from the developing property to less than 80% of the peak flows calculated for pre-development conditions, and remain operational until the downstream storm drain facilities are fully constructed.

OFF-SITE FLOWS

Storm water runoff from the City of Ontario enters the Study Area from the north. Ultimate 100-year storm runoff hydrographs for Ontario's master planned storm drains, per Ontario's Master Plan of Drainage for New Model Colony prepared by L.D. King, Inc., have been incorporated in this study for conveyance to downstream regional drainage facilities. Ontario's master planned storm drains enter the Study Area at three locations as follows:

1. LINE "A": A 14'(wide) x 8'(high) RC Box storm drain is proposed to enter the Study Area at the intersection of Merrill Avenue and Baker Avenue, conveying storm runoff from approximately 1,362 acres with a peak flow of 1,620 cfs.
2. LINE "J": A 108" RCP storm drain in Grove Avenue, with a 72" RCP lateral storm drain in Merrill Avenue, is proposed to drain to the existing 10'(wide) x 6'(high) TEC Grove Avenue Storm Drain Channel. This storm drain system will have a peak design flow of 1,227 cfs as it enters the Study Area, with a tributary drainage area of approximately 850 acres.
3. LINE "I": A 10'(wide) x 8'(high) RC Box storm drain in Merrill Avenue and an 84" RCP storm drain in Euclid Avenue are proposed to confluence and drain to the existing Airport Channel along Euclid Avenue. This storm drain system will have a peak design flow of 1,443 cfs as it enters the City of Chino, with a tributary drainage area of approximately 1,840 acres. The Airport Channel enters the Study Area at the intersection of Euclid Avenue and Kimball Avenue with a peak flow of 1,845.21 cfs and a tributary drainage area of 2,277 acres.

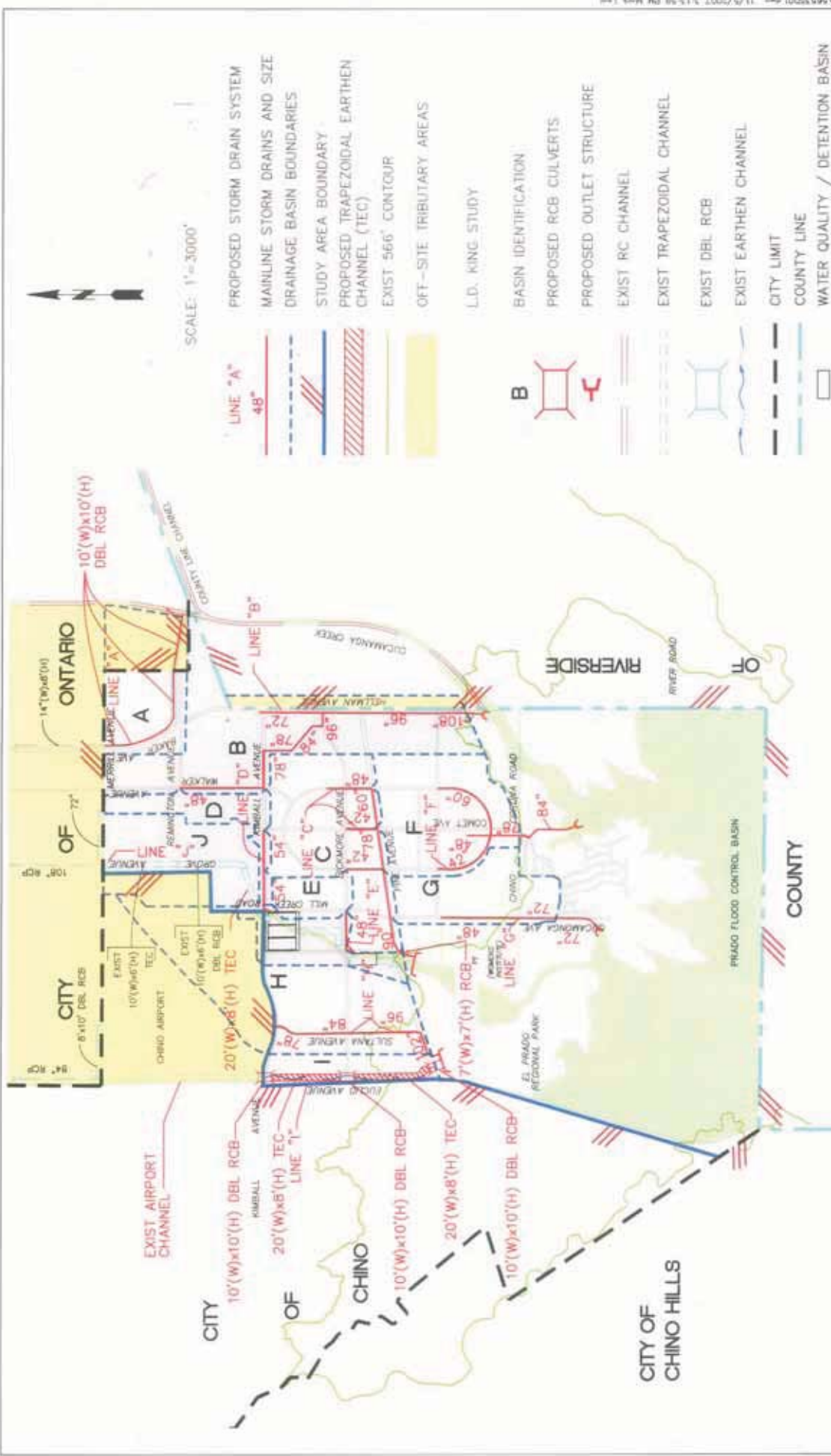
the outlet should equal as closely as possible with the existing channel velocity. When the discharge velocity is low or sub-critical, the outlet structures shall consist of a headwall, wing-walls, and apron. When the discharge velocity is high or supercritical, an appropriate energy dissipater and bank protection structure shall be designed in the vicinity of the outlet.

10. If development occurs in the upstream areas prior to construction of the downstream storm drain facilities, local detention basin(s) should be implemented to handle the additional flows generated from such development. The detention basins shall be designed to retard the discharge from the developing property to less than 80% of the peak flows calculated for pre-development conditions, and remain operational until the downstream storm drain facilities are fully constructed.

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1. LINE "A": A 14'(wide) x 8'(high) RC Box storm drain is proposed to enter the Study Area at the intersection of Merrill Avenue and Baker Avenue, conveying storm runoff from approximately 1,362 acres with a peak flow of 1,620 cfs.
2. LINE "J": A 108" RCP storm drain in Grove Avenue, with a 72" RCP lateral storm drain in Merrill Avenue, is proposed to drain to the existing 10'(wide) x 6'(high) TEC Grove Avenue Storm Drain Channel. This storm drain system will have a peak design flow of 1,227 cfs as it enters the Study Area, with a tributary drainage area of approximately 850 acres.
3. LINE "I": A 10'(wide) x 8'(high) RC Box storm drain in Merrill Avenue and an 84" RCP storm drain in Euclid Avenue are proposed to confluence and drain to the existing Airport Channel along Euclid Avenue. This storm drain system will have a peak design flow of 1,443 cfs as it enters the City of Chino, with a tributary drainage area of approximately 1,840 acres. The Airport Channel enters the Study Area at the intersection of Euclid Avenue and Kimball Avenue with a peak flow of 1,845.21 cfs and a tributary drainage area of 2,277 acres.



SCALE: 1"=3000'

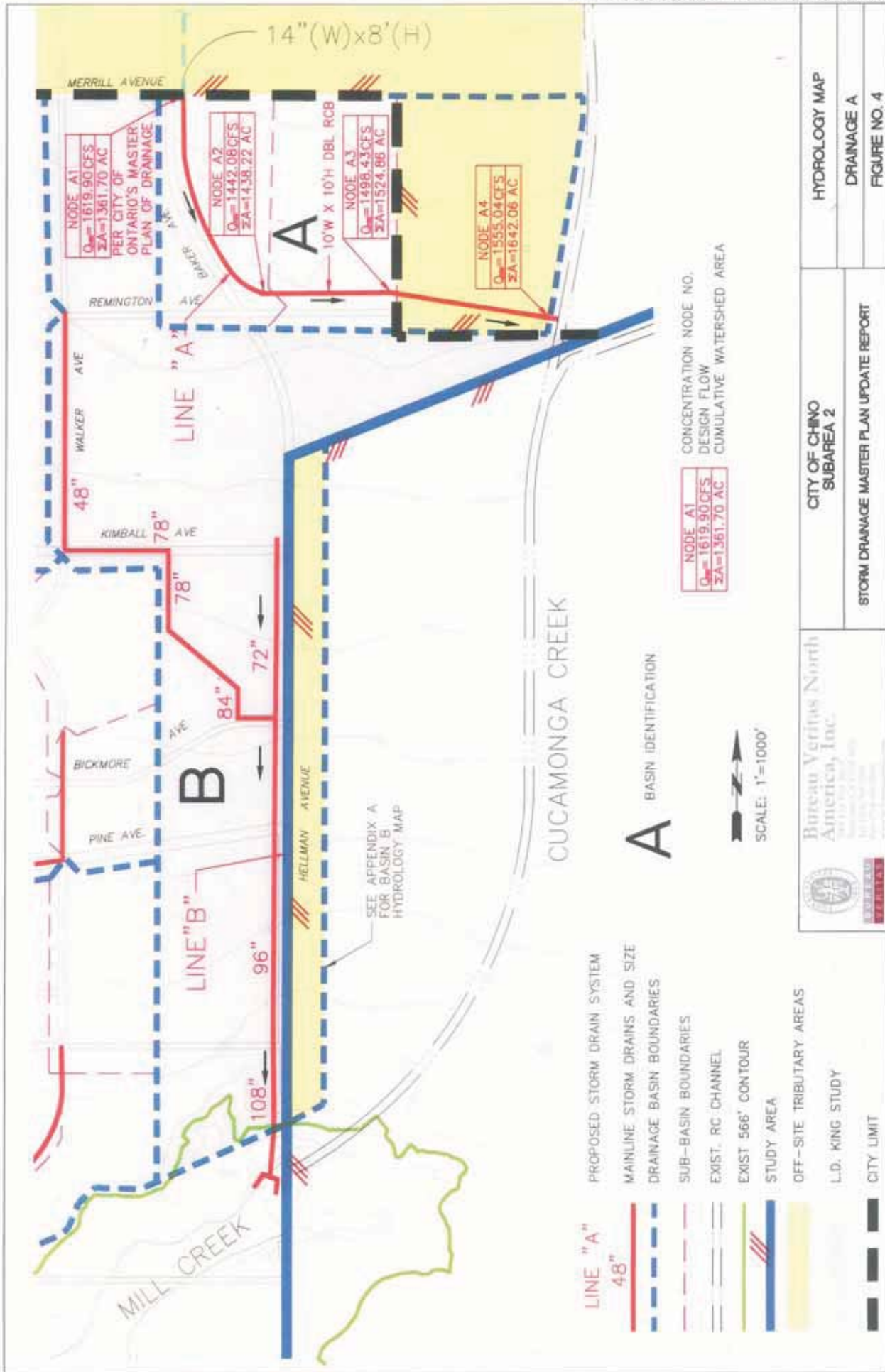
- PROPOSED STORM DRAIN SYSTEM
- MAINLINE STORM DRAINS AND SIZE
- DRAINAGE BASIN BOUNDARIES
- STUDY AREA BOUNDARY
- PROPOSED TRAPEZOIDAL EARTHEN CHANNEL (TEC)
- EXIST 566' CONTOUR
- OFF-SITE TRIBUTARY AREAS
- L.D. KING STUDY
- BASIN IDENTIFICATION
- PROPOSED RCB CULVERTS
- PROPOSED OUTLET STRUCTURE
- EXIST RC CHANNEL
- EXIST TRAPEZOIDAL CHANNEL
- EXIST DBL RCB
- EXIST EARTHEN CHANNEL
- CITY LIMIT
- COUNTY LINE
- WATER QUALITY / DETENTION BASIN

CITY OF CHINO
SUBAREA 2

STORM DRAINAGE MASTER PLAN UPDATE REPORT

DRAINAGE BASIN BOUNDARY MAP
FIGURE NO. 3





Line "A" will start at the terminus of Ontario's planned storm drain "WALK-A1" at Merrill Avenue, and run south in the proposed new alignment of Hellman Avenue from Merrill Avenue to Remington Avenue; thence turn east along Remington Avenue to the Cucamonga Creek Channel. This storm drain system will convey storm runoff from approximately 163 acres of Basin A, and runoff from approximately 1,362 acres of the City of Ontario's New Model Colony. Basin A is bounded by Merrill Avenue to the north, Chino City Limit Line to the east, Realigned Baker/Hellman Avenue to the west, and Remington Avenue to the south.

LINE "B":

Line "B" will convey storm runoff from Drainage Basin B to the Prado Basin, as shown in the Basin B Hydrology Map by L.D. King (included in Appendix A). The Basin B is comprised of approximately 580 acres bounded by Hellman Avenue to the east, Basin A and Merrill Avenue to the north, Walker Avenue and Baker Avenue to the west, and Prado Basin to the south.

Line "B" is comprised of approximately 13,950 linear feet of 48 to 108 inch RCP storm drain total Capital Cost of \$10.93 million.

LINE "C" and LINE "E":

Lines "C", and "E", as shown in Figure 5, are proposed storm drain systems serving Drainage Basins C and E bounded by Kimball Avenue to the north, Baker Avenue to the east, Pine Avenue to the south, and Cucamonga Avenue to the west. These storm drain systems convey stormwater flows in Pine Avenue and Bickmore Avenue to a watercourse in the Prado Basin.

Line "C" is comprised of approximately 7,430 feet of 48 inch RCP to 7'x7' RCB and lateral storm drains with an estimated Project Capital Cost of \$6.75 million.

Line "E" is approximately 1,600 feet of 48 inch RCP storm drain in Bickmore Avenue with an estimated Project Capital Cost of \$0.81 million.

LINE "D" and Line "J":

Storm Drain Lines "D" and "J" are based on the L.D. King Study serving Drainage Basins D and J, as shown in the Hydrology Map by L.D. King, included in Appendix A. Drainage Basins D and J are comprised of approximately 2,610 acre area bounded by Walker Avenue, Cucamonga Avenue and Rincon Meadows Avenue (Basins B, C and E) to the east, Merrill Avenue (City of Ontario) to the north, Basins H and I to the west, and Prado Basin to the south.

Line "D" is comprised of approximately 3,280 linear feet of 54-inch RCP storm drain total Capital Cost of \$1.73 million.

Line "J" is an existing storm drain system that begins at the Bickmore WQMP Basin adjacent to the Prado Basin, and extends north-easterly as a 8'x 5' double barrel RCB, and open trapezoidal channel to the Kimball Avenue Detention Basins located at the southwest corner of Kimball Avenue and Mill Creek Road, thence extends north through the Chino Airport as 10'x 6' double barrel RCB and open trapezoidal channel to Merrill Avenue, thence north in Grove Avenue in the City of Ontario.

LINE "F" and LINE "G":

Storm Drain Lines "F" and "G", as shown in Figure 6, are storm drain systems proposed to service the developable portions of the Study Area that lie to the south of Pine Avenue and east of Cucamonga Avenue, including portions of the proposed Edgewater Development. These storm drains convey tributary flows southerly to the Prado Basin.

Line "F" is comprised of approximately 8,700 feet of 42 to 84 inch RCP mainline and lateral storm drains with an estimated Project Capital Cost of \$5.13 million.

Line "G" is approximately 5,200 feet of 48 to 72 inch RCP storm drain in Cucamonga Avenue with an estimated Project Capital Cost of \$3.21 million for City of Chino.

LINE "H":

Storm Drain Line "H", as shown in Figure 7 is an approximately 6,000 feet, 78 to 102 inch diameter storm drain system in Pine Avenue, Bickmore Avenue and Sultana Avenue, with an estimated total Capital Cost of \$5.17 million for City of Chino. Starting at Kimball Avenue, the proposed storm drain will run south in Sultana Avenue to drain into the natural watercourse south of Pine Avenue, east of Euclid Avenue. It is projected to receive flows from an approximately 287-acre area of Chino Airport and 308 acres from Drainage Basin H.

LINE "I":

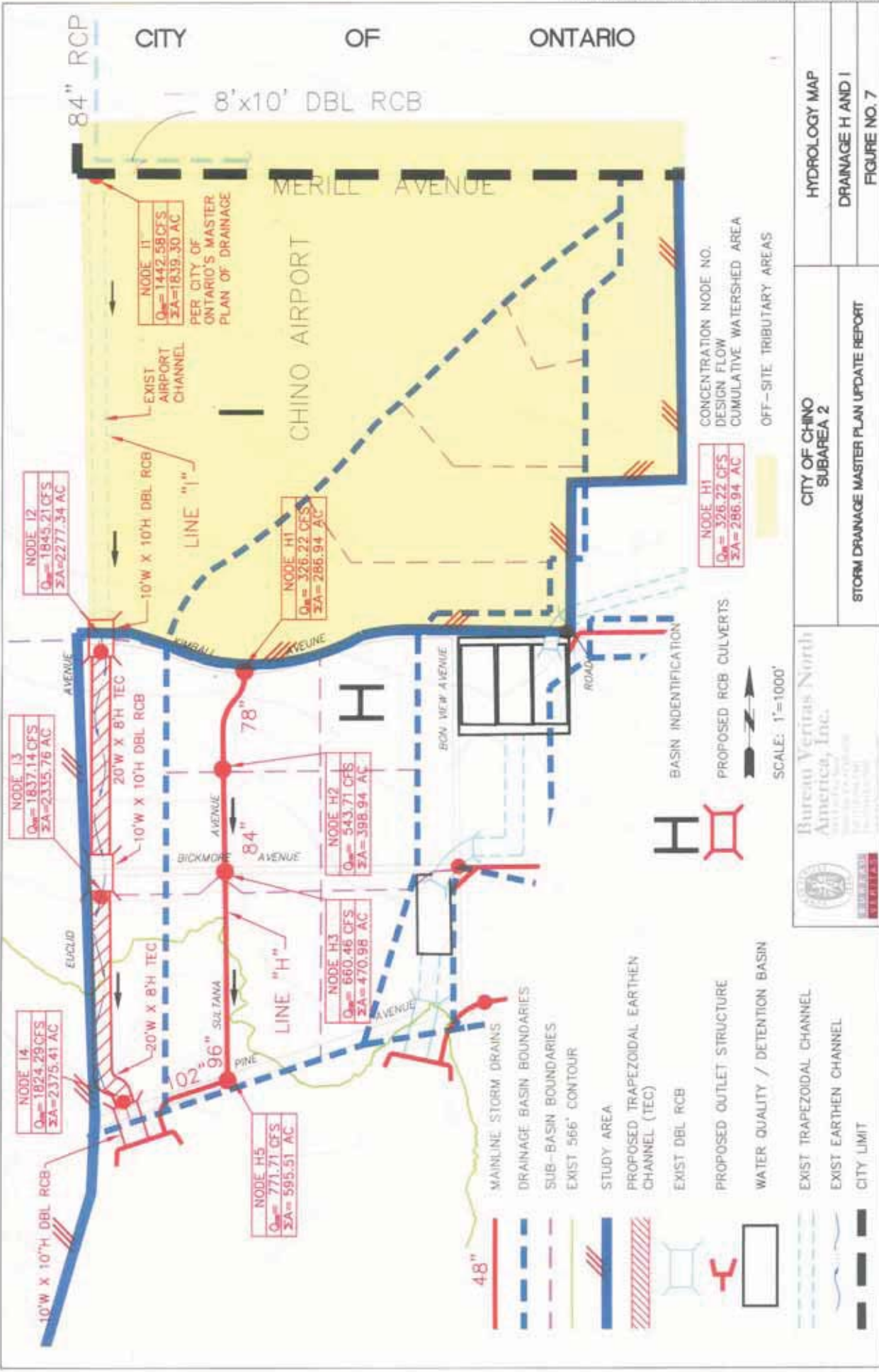
Drainage Basin "I" is presently served by an existing drain along Euclid Avenue. This drain is comprised of an unimproved, under-capacity earthen ditch along the easterly side of Euclid Avenue from Pine Avenue to Kimball Avenue, and an improved trapezoidal earthen channel (Airport Channel) from Kimball Avenue to Merrill Avenue.

Three alternative options were evaluated for this drain.

Option 1: An improved earthen trapezoidal channel, downstream from the Airport Channel, from Kimball Avenue to the natural watercourse south of Pine Avenue, with RCB culvert crossings under Kimball Avenue, Bickmore Avenue and Pine Avenue is the most cost effective and recommended option. Assuming that the channel could be constructed within the 200-foot wide existing street right-of-way, the estimated Capital Cost for this Option is \$2.45 million. The estimated Capital Cost share for City of Chino and City of Ontario is \$0.59 million and \$1.96 million, respectively.

Option 2: A concrete-lined trapezoidal channel from the outlet south of Pine Avenue, to Merrill Avenue, with RCB crossings at Kimball Avenue, Bickmore Avenue and Pine Avenue would have a Capital Cost estimate of \$10.10 million.

Option 3: An underground RCB storm drain from the outlet south of Pine Avenue to Merrill Avenue would have a total estimated Capital Cost of \$15.65 million.



CITY OF CHINO SUBAREA 2

STORM DRAINAGE MASTER PLAN UPDATE REPORT

HYDROLOGY MAP DRAINAGE H AND I

FIGURE NO. 7

Bureau Veritas North America, Inc.

REGISTERED PROFESSIONAL ENGINEER

STATE OF CALIFORNIA

NO. 45678

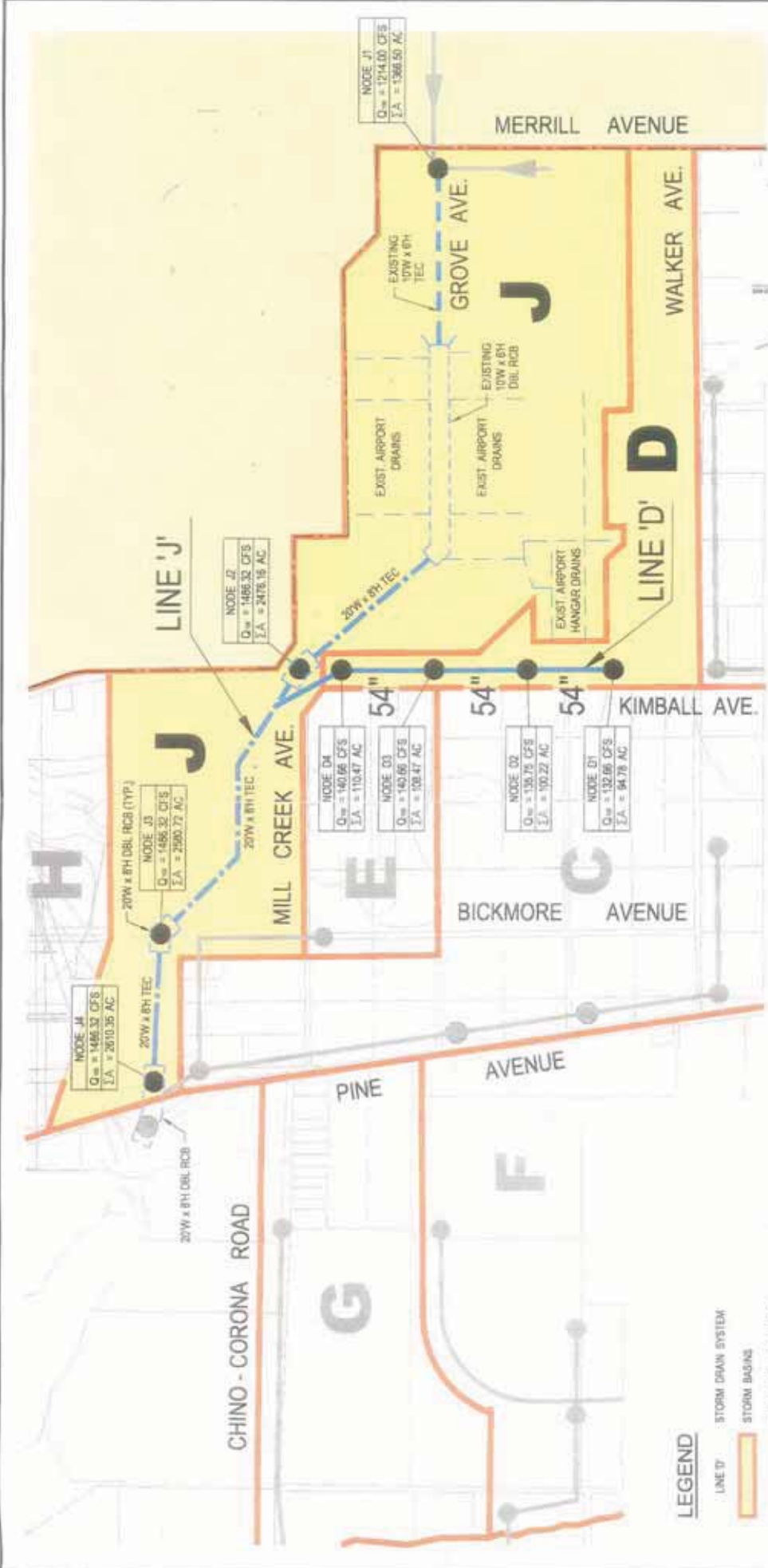
COST ESTIMATES

Presented in Appendix C is a detailed breakdown of construction quantities and capital costs for the recommended storm drain systems. Estimates for construction and project costs have been developed using February 2007 construction costs, based on ENR Construction Cost Index of 7,864.7 for the recommended storm drain facilities shown on the Basin Hydrology Maps.

The Construction Costs incorporate a contingency of 20% and the Capital Costs includes 10% of Construction Costs for engineering and administration.

APPENDIX A

HYDROLOGY MAPS BY L.D. KING



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 21511 Convention Center Way
 Suite 1018
 Culver City, California 91714-4684
 Phone: (805) 937-0200
 Fax: (805) 937-0202



LCKING
 Engineers/Planners/Surveyors

AMENDMENT TO HYDROLOGY MAP BASINS D & J

LEGEND

- LINE D' STORM DRAIN SYSTEM
 - STORM BASINS
 - STUDY AREA BOUNDARY
 - OFF-SITE TRIBUTARY AREAS
 - DRAINAGE BASIN IDENTIFICATION
 - MAJOR STORM DRAINS
 - DOUBLE RCB
 - TRAPEZOIDAL EARTHEN CHANNEL (TEC)
 - EXISTING STORM DRAIN
- | NODE XXX | CONCENTRATION | NODE NO. |
|-------------------------------|---------------------------|----------|
| Q _{des} = 100.00 CFS | DESIGN FLOW | |
| E.A. = 000.00 AC | CUMULATIVE WATERSHED AREA | |

8/15/11 11:48 AM

APPENDIX B
FACILITY DATA

TABLE 1: FACILITY DATA

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2

LINE #	NODE		LENGTH ft	ELEVATION		GROUND SLOPE ft/ft	DESIGN SLOPE ft/ft	HYDRAULIC GRADIENT ft/ft	Q10 cfs	Q25 cfs	Q100 cfs	DESIGN FLOW cfs	K _s -CIP-5	PIPE SIZE in	BOX SIZE DBL PCB	CHANNEL SIZE ft x ft	VELOCITY CFS
	FROM #	TO #		ft	ft												
A	A1	A2	2800	660.5	645	0.0055357	0.0021	0.001785	1620	1620	1620	1620	38343.867		10' W X 10' H		9.64
	A2	A3	1400	645	643	0.0014286	0.0021	0.001785	1620	1620	1620	1620	38343.867		10' W X 10' H		9.64
	A3	A4	1700	643	640	0.0017647	0.0021	0.001785	1620	1620	1620	1620	38343.867		10' W X 10' H		9.64
	A4	OUTLET	100	640	638	0.02	0.0021	0.001785	1620	1620	1620	1620	38343.867		10' W X 10' H		9.64

B SEE AMENDMENT TO MASTER PLAN OF DRAINAGE FOR SUBAREA 2, PREPARED BY L.D. KING, DATED JULY 8, 2004 (INCLUDED IN APPENDIX B)

C	C1	C2	1450	610	602	0.0055172	0.0065	0.005525	95	116	95	95	1278.0783	48			9.58
	C2	C3	1300	602	595	0.0053846	0.0065	0.005525	152	187	152	187	2515.7962	60			11.2
	C3	C5	1350	595	590	0.0037037	0.0065	0.005525	270	335	270	335	4506.9077	78			13.18
	C5	C7	2380	590	572	0.007563	0.0065	0.005525	405	502	405	502	6753.6349	90			14.54
	C7	OUTLET	950	572	570	0.0021053	0.0065	0.005525	472	586	472	586	7883.7251		7' W X 7' H		12.96
	C4	C3	1200	608	595	0.0108333	0.008	0.006800	58	67	58	67	703.35331	42			9.33
	C6	C5	1250	600	590	0.008	0.008	0.006800	82	96	82	96	994.39606	42			9.83

D SEE AMENDMENT TO MASTER PLAN OF DRAINAGE FOR SUBAREA 2, PREPARED BY L.D. KING, DATED JULY 8, 2004 (INCLUDED IN APPENDIX B)

TABLE 1: FACILITY DATA

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2

LINE #	NODE		LENGTH ft	ELEVATION		GROUND SLOPE ft/ft	DESIGN SLOPE ft/ft	HYDRAULIC GRADIENT ft/ft	Q10		DESIGN FLOW cfs	K _s Q ^{1.49} S ^{4.75}	PIPE SIZE in	BOX SIZE INR - HCL ft X ft	CHANNEL SIZE ft X ft	VELOCITY	
	FROM	TO		U/S ft	D/S ft				cfs	ft/s						cfs	ft/s
E	E1	OUTLET	1606	594	580	0.00875	0.0101	0.008585	115	142	115	1241.1598	48				
F	F1	F2	2500	576.5	572	0.0018	0.002	0.001700	31	41	31	751.86044	42				4.73
	F3	F2	900	575	572	0.00333333	0.002	0.001700	48	53	48	1164.171	48				5.25
	F4	F2	2500	582	572	0.004	0.002	0.001700	95	126	95	2304.0884	60				6.17
	F2	F5	900	572	566	0.00666667	0.006	0.005100	298	391	298	4172.8347	78				12.52
	F5	F6	700	566	561	0.0071429	0.008	0.006800	374	519	374	6293.7995	84				15.6
	F6	OUTLET	1200	561	545	0.01333333	0.01	0.008500	570	570	570	6182.518	84				17.43
G	G1	G2	2200	574.9	565	0.0045	0.003	0.002550	73	95	73	1445.6154	48				6.64
	G2	G3	1500	565	560	0.00333333	0.005	0.004500	174	235	174	3604.7354	72				10.9
	G3	OUTLET	1500	560	545	0.01	0.01	0.008500	210	294	204	3188.6777	72				15.16
H	H1	H2	1500	594	583	0.00733333	0.0075	0.006375	326	423	326	4082.9824	78				13.97
	H2	H3	1000	583	571	0.012	0.0075	0.006375	419	544	444	6813.3203	84				14.95
	H3	H5	2300	571	565	0.0026087	0.0075	0.006375	509	660	660	8266.1606	96				16.43
	H5	OUTLET	1200	565	550	0.0125	0.0075	0.006375	590	772	772	9668.9031	102				17.01

EARTHEN TRAPEZOIDAL CHANNEL (OPTION 1)

I	I2	I3	2900	595	570.5	0.0084483	0.007		1891	1891	1891				20' W X 8' H		19.53
	I3	I4	2500	570.5	557	0.0054	0.007		1924	1924	1924				20' W X 8' H		19.63
	I2	I2	120				0.007	0.007000	1891	1891	1891	22601.773			DBL 10' W X 10' H		16.95
	I3	I3	100				0.007	0.007000	1924	1924	1924	22996.198			DBL 10' W X 10' H		17.02
	I4	OUTLET	500	557	540	0.034	0.02	0.02	1932	1932	1932	13661.903			DBL 10' W X 10' H		25.17

TABLE 1: FACILITY DATA

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2																	
LINE #	MODE		LENGTH ft	ELEVATION		GROUND SLOPE 1/ft	DESIGN SLOPE 1/ft	HYDRAULIC GRADIENT ft/ft	O 10 dia	O 25 dia	O 100 dia	DESIGN FLOW cfs	K _s O/SK _s E	PIPE SIZE in	BOX SIZE DBL. RCB ft X ft	CHANNEL SIZE ft X ft	VELOCITY CFS fs
	FROM #	TO #		U/S ft	D/S ft												
CONCRETE TRAPEZOIDAL CHANNEL (OPTION 2)																	
1	11	12	5250	535	595	0.007619	0.007				1443	1443				20' W X 5' H	17.93
1	12	13	2840	595	570.5	0.0086268	0.007				1891	1891				20' W X 8' H	19.53
	13	14	2190	570.5	557	0.0061644	0.007				1924	1924				20' W X 8' H	19.63
	12	CULVER					0.007	0.007000			1891	1891	22601.773			DBL 10' W X 10' H	16.95
	13	CULVER					0.007	0.007000			1924	1924	22996.198			DBL 10' W X 10' H	17.02
	14	CULVER	500	557	540	0.034	0.02				1932	1932	13691.303			DBL 10' W X 10' H	25.17
REINFORCED CONCRETE BOX (OPTION 3)																	
1	11	12	5300	635	595	0.0075472	0.007	0.005950			1443	1443	18707.159			DBL 11' W X 6' H	14.92
	12	13	2900	595	570.5	0.0084483	0.007	0.005950			1891	1891	24515.065			DBL 11' W X 6' H	16
	13	14	2500	570.5	557	0.0054	0.007	0.005950			1924	1924	24942.879			DBL 11' W X 6' H	14.57
	14	OUTLET	500	557	551	0.012	0.007	0.005950			1932	1932	25046.592			DBL 11' W X 6' H	14.64

TABLE 1D: FACILITY DATA
 AMENDMENT NO. 1

MASTER PLAN OF DRAINAGE - CHINO SPHERE OF INFLUENCE - SUBAREA 2

LINE #	NODE		LENGTH		ELEVATION		GROUND SLOPE		DESIGN SLOPE		HYDRAULIC GRADIENT		Q		DESIGN FLOW		K _s -Q _s ⁿ -S		PIPE SIZE		BOX SIZE		CHANNEL SIZE		
	FROM #	TO #	ft	ft	ft	ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft	ft/ft
D	D1	D2	870	823.3	620.5	0.00322989	0.0025	0.002126	90	107	133	2885.175089	54												
	D2	D3	940	620.5	617.5	0.00317021	0.0025	0.002125	93	109	136	2950.254225	54												
	D3	D4	1320	617.5	600.5	0.01290909	0.0025	0.002125	96	113	141	3058.719455	54												
	D4	OUTLET	150	600.5	584.3	0.04146667	0.0025	0.002126	96	113	141	3058.719455	54												

APPENDIX C

CAPITAL COST ESTIMATES

TABLE 1: CAPITAL COST ESTIMATE SUMMARY

STORM DRAIN MASTER PLAN UPDATE CITY OF CHINO - SUBAREA 2			
LINE	CITY OF CHINO CAPITAL COST	CITY OF ONTARIO CAPITAL COST	TOTAL CAPITAL COST
A		\$ 18,302,000	\$ 18,302,000
B	\$ 10,928,720		\$ 10,928,720
C	\$ 6,745,926		\$ 6,745,926
D	\$ 1,728,584		\$ 1,728,584
E	\$ 805,200		\$ 805,200
F	\$ 5,126,990		\$ 5,126,990
G	\$ 3,204,300		\$ 3,204,300
H	\$ 5,167,250		\$ 5,167,250
I	\$ 561,255	\$ 1,878,985	\$ 2,440,240
TOTAL COST	\$ 34,268,225	\$ 20,180,985	\$ 54,449,210

TABLE 2: CAPITAL COST ESTIMATE

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2

LINE #	NODE		SIZE	LENGTH ft	CONST. COST		ENGR. ADMIN	TOTAL COST	TOTAL CAPITAL COST	CITY OF CHINO		CITY OF ONTARIO
	FROM	TO			CONST. COST	S&LF				CAPITAL COST	0% COST	
A.	MERRILL AVE	CUCAMONGA CREEK	10' (W) X 10' (H) DBL RCB	5000	2,720	\$ 16,320,000	\$ 1,632,000	\$ 17,952,000	\$ 17,952,000			\$ 17,952,000
	40" WIDE DRAINAGE EASMENT											
TOTAL CAPITAL COST =									\$ 18,302,000	\$ 350,000	\$ 18,302,000	\$ 350,000

TABLE 3: CAPITAL COST ESTIMATE

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2												
LINE #	NODE		SIZE	LENGTH	CONST. COST		ENGR/ADMIN	TOTAL COST	TOTAL CAPITAL COST			
	FROM	TO			CONST. COST	3/LF				ENGR/ADMIN	ENGR/ADMIN	ENGR/ADMIN
B	B1	B2	48" RCP	2650	445	\$ 1,176,250	\$ 117,925	\$ 1,294,175				
	B2	B3	76" RCP	900	593	\$ 623,700	\$ 62,370	\$ 686,070				
	B3	B4	76" RCP	1350	603	\$ 935,550	\$ 93,555	\$ 1,029,105				
	B4	B5	84" RCP	1050	768	\$ 806,400	\$ 80,640	\$ 887,040				
	B5	B7	84" RCP	600	768	\$ 460,800	\$ 46,080	\$ 506,880				
	B6	B7	72" RCP	2300	638	\$ 1,467,400	\$ 146,740	\$ 1,614,140				
	B7	B8	96" RCP	900	828	\$ 745,200	\$ 74,520	\$ 819,720				
	B8	B9	96" RCP	2500	828	\$ 2,070,000	\$ 207,000	\$ 2,277,000				
	B9	B10	108" RCP	900	957	\$ 861,300	\$ 86,130	\$ 947,430				
	B10	OUTLET	108" RCP	500	957	\$ 765,800	\$ 76,580	\$ 842,380				
OUTLET STRUCTURE					\$ 20,000	\$ 2,000	\$ 22,000				\$ 10,928,720.00	
C	C1	C2	48" RCP	1450	445	\$ 645,250	\$ 64,525	\$ 709,775				
	C2	C3	60" RCP	1300	532	\$ 691,600	\$ 69,160	\$ 760,760				
	C3	C5	78" RCP	1350	683	\$ 935,550	\$ 93,555	\$ 1,029,105				
	C5	C7	90" RCP	2380	807	\$ 1,920,660	\$ 192,066	\$ 2,112,726				
	C7	OUTLET	7" W X 7" H RCB	950	1020	\$ 969,000	\$ 96,900	\$ 1,065,900				
	C4	C3	42" RCP	1200	388	\$ 465,600	\$ 46,560	\$ 512,160				
OUTLET STRUCTURE	C6	C5	42" RCP	1250	388	\$ 485,000	\$ 48,500	\$ 533,500				
					\$ 20,000	\$ 2,000	\$ 22,000				\$ 6,745,926.00	
D	D1	D2	54" RCP	670	473	\$ 411,510	\$ 41,151	\$ 452,661				
	D2	D3	54" RCP	940	473	\$ 444,620	\$ 44,462	\$ 489,082				
	D3	D4	54" RCP	1320	473	\$ 624,360	\$ 62,436	\$ 686,796				
	D4	OUTLET	54" RCP	150	473	\$ 70,950	\$ 7,095	\$ 78,045				
	OUTLET STRUCTURE					\$ 20,000	\$ 2,000	\$ 22,000				\$ 1,728,584.00

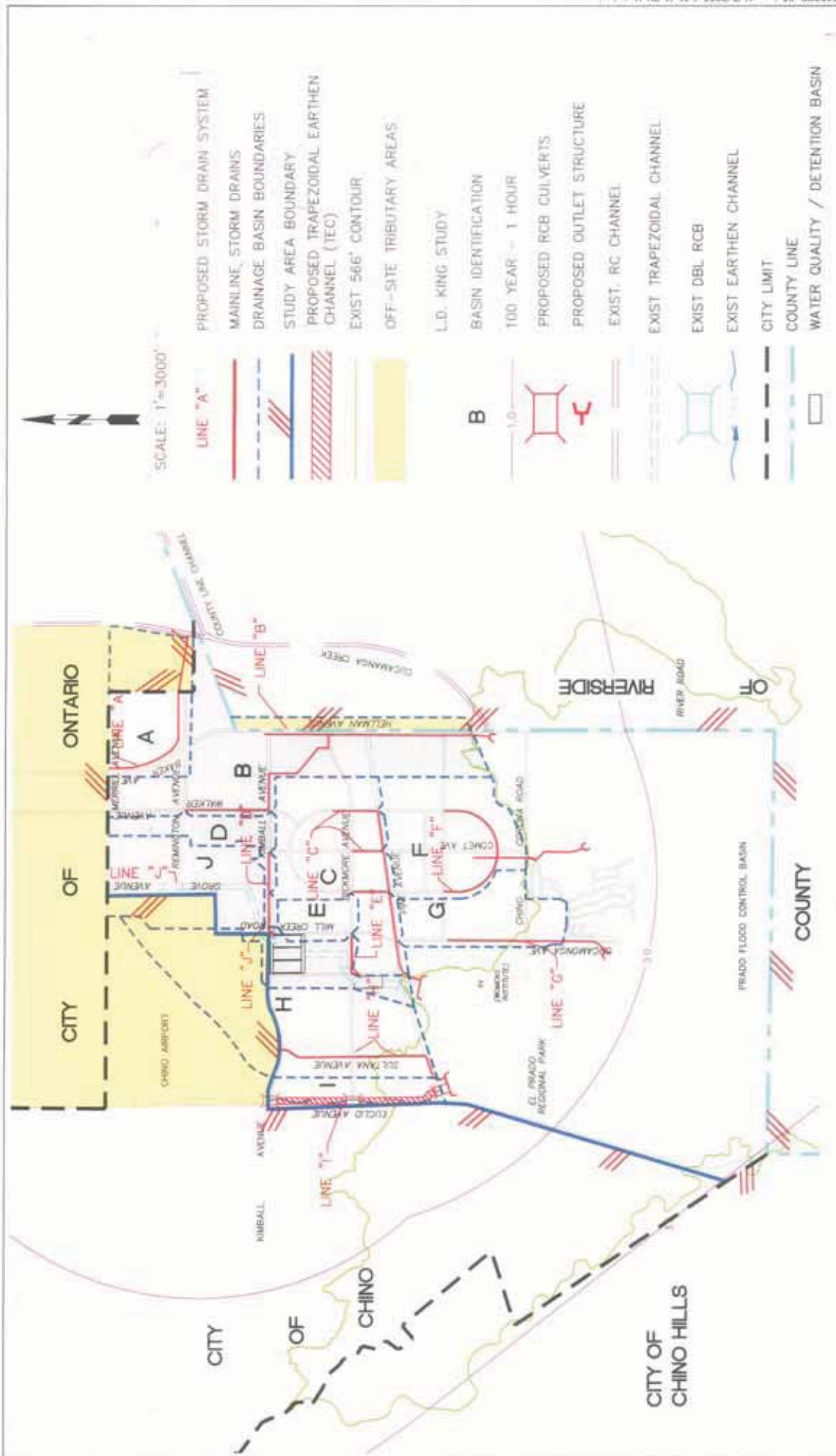
TABLE 3: CAPITAL COST ESTIMATE

STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2										
LINE	FROM	TO	SIZE	LENGTH	CONST COST \$/LF	CONST COST	ENGR/ADMIN	TOTAL COST	TOTAL CAPITAL COST	
E	E1	E2	48" RCP	1600	445	\$ 712,000	\$ 71,200	\$ 783,200		
OUTLET STRUCTURE						\$ 20,000	\$ 2,000	\$ 22,000		\$ 905,200.00
F	F1	F2	42" RCP	2500	388	\$ 970,000	\$ 97,000	\$ 1,067,000		
	F3	F2	48" RCP	900	445	\$ 400,500	\$ 40,050	\$ 440,550		
	F4	F2	60" RCP	2500	532	\$ 1,330,000	\$ 133,000	\$ 1,463,000		
	F2	F5	78" RCP	900	693	\$ 623,700	\$ 62,370	\$ 686,070		
	F5	F6	84" RCP	700	693	\$ 485,100	\$ 48,510	\$ 533,610		
	F6	OUTLET	84" RCP	1200	693	\$ 831,600	\$ 83,160	\$ 914,760		
OUTLET STRUCTURE						\$ 20,000	\$ 2,000	\$ 22,000		\$ 5,126,990.00
G	G1	G2	48" RCP	2200	445	\$ 979,000	\$ 97,900	\$ 1,076,900		
	G2	G3	72" RCP	1500	638	\$ 957,000	\$ 95,700	\$ 1,052,700		
OUTLET STRUCTURE		OUTLET	72" RCP	1500	638	\$ 957,000	\$ 95,700	\$ 1,052,700		
						\$ 20,000	\$ 2,000	\$ 22,000		\$ 3,204,300.00
H	H1	H2	78" RCP	1500	693	\$ 1,039,500	\$ 103,950	\$ 1,143,450		
	H2	H3	84" RCP	1000	693	\$ 693,000	\$ 69,300	\$ 762,300		
	H3	H5	96" RCP	2300	828	\$ 1,904,400	\$ 190,440	\$ 2,094,840		
	H5	OUTLET	102" RCP	1200	663	\$ 1,035,600	\$ 103,560	\$ 1,139,160		
OUTLET STRUCTURE						\$ 25,000	\$ 2,500	\$ 27,500		\$ 5,167,250.00
									TOTAL CAPITAL COST =	\$ 33,706,970.00

TABLE 4: CAPITAL COST ESTIMATE

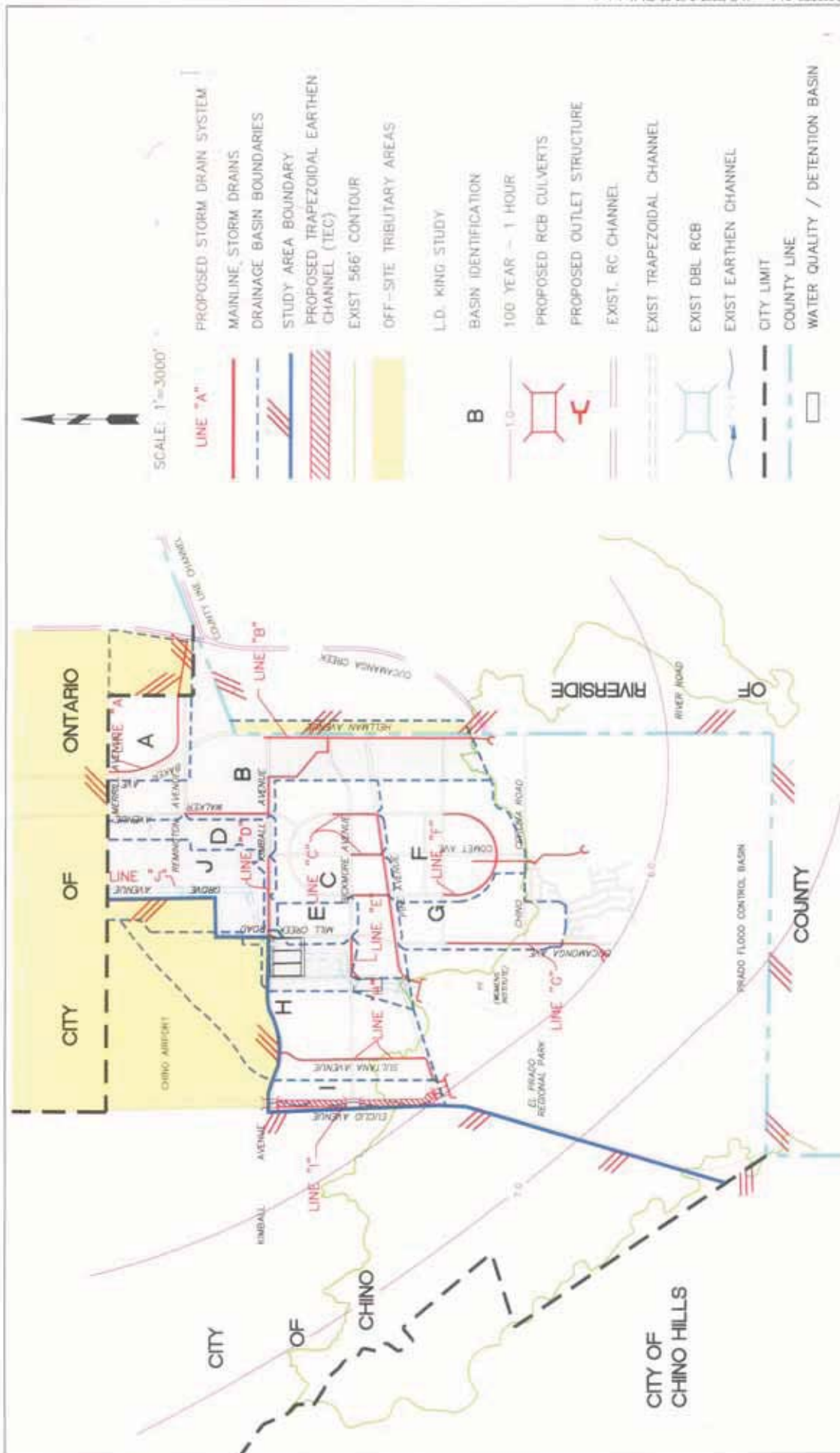
STORM DRAIN MASTER PLAN UPDATE - CITY OF CHINO - SUBAREA 2													
LINE	FROM	NODE	TO	SIZE	LENGTH	CONST. COST	ENGR. ADMIN. COST	TOTAL CAPITAL COST	CITY OF CHINO CAPITAL COST	CITY OF ONTARIO CAPITAL COST			
#					ft.	\$/L.F.			23% COST	77% COST			
EARTHEN TRAPEZOIDAL CHANNEL (OPTION 1)													
1	MERRILL	KIMBALL		EXISTING CHANNEL									
	I-2		I-3	20' (W) X 8' (H) TEC	2900	300 \$	870,000 \$	87,000 \$	957,000 \$	220,110 \$	736,890 \$		
	I-3		I-4	20' (W) X 8' (H) TEC	2500	300 \$	750,000 \$	75,000 \$	825,000 \$	189,750 \$	635,250 \$		
	I-2			10' (W) X 10' (H) DBL RCB	120	2,720 \$	326,400 \$	32,640 \$	359,040 \$	82,579 \$	276,461 \$		
	I-3			10' (W) X 10' (H) DBL RCB	100	2,720 \$	272,000 \$	27,200 \$	299,200 \$	68,816 \$	230,384 \$		
	I-4			10' (W) X 10' (H) DBL RCB	500	2,720 \$	1,360,000 \$	136,000 \$	1,496,000 \$	344,080 \$	1,151,920 \$		
TOTAL CAPITAL COST =								\$	2,440,240 \$	\$	561,255 \$	\$	1,878,985 \$
CONCRETE TRAPEZOIDAL CHANNEL (OPTION 2)													
1	I-1		I-2	20' (W) X 5' (H) TCC	5250	1,700 \$	8,925,000 \$	892,500 \$	9,817,500 \$	2,258,025 \$	7,559,475 \$		
	I-2		I-3	20' (W) X 6' (H) TCC	2840	1,700 \$	4,828,000 \$	482,800 \$	5,310,800 \$	1,221,484 \$	4,089,316 \$		
	I-3		I-4	20' (W) X 6' (H) TCC	2190	1,700 \$	3,723,000 \$	372,300 \$	4,095,300 \$	941,919 \$	3,153,381 \$		
	I-2			10' (W) X 10' (H) DBL RCB	120	2,720 \$	326,400 \$	32,640 \$	359,040 \$	82,579 \$	276,461 \$		
	I-3			10' (W) X 10' (H) DBL RCB	100	2,720 \$	272,000 \$	27,200 \$	299,200 \$	68,816 \$	230,384 \$		
	I-4			10' (W) X 10' (H) DBL RCB	500	2,720 \$	1,360,000 \$	136,000 \$	1,496,000 \$	344,080 \$	1,151,920 \$		
TOTAL CAPITAL COST =								\$	10,064,340 \$	\$	2,314,798 \$	\$	7,749,542 \$
REINFORCED CONCRETE BOX (OPTION 3)													
1	I-1		I-2	11' (W) X 6' (H) DBL RCB	5300	2,410 \$	12,773,000 \$	1,277,300 \$	14,050,300 \$	3,231,569 \$	10,818,731 \$		
	I-2		I-3	11' (W) X 6' (H) DBL RCB	2800	2,410 \$	6,989,000 \$	698,900 \$	7,687,900 \$	1,766,217 \$	5,919,683 \$		
	I-3		I-4	11' (W) X 6' (H) DBL RCB	2500	2,410 \$	6,025,000 \$	602,500 \$	6,627,500 \$	1,524,325 \$	5,103,175 \$		
	I-4			11' (W) X 6' (H) DBL RCB	500	2,410 \$	1,205,000 \$	120,500 \$	1,325,500 \$	304,865 \$	1,020,635 \$		
TOTAL CAPITAL COST =								\$	15,640,900 \$	\$	3,597,407 \$	\$	12,043,493 \$

ISOHYETAL MAPS



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CITY OF CHINO SUBAREA 2		ISOHYETALS 100 YEAR - 6 HOUR
STORM DRAINAGE MASTER PLAN UPDATE REPORT		FIGURE NO. 9



<p>STORM DRAINAGE MASTER PLAN UPDATE REPORT</p>	<p>CITY OF CHINO SUBAREA 2</p>	<p>ISCHYETALS 100 YEAR - 24 HOUR</p>
	<p>FIGURE NO. 10</p>	

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